

Optimal Sitting and Sizing of Distributed Generation Units in an Indian Practical Distribution System using Bird Swarm Algorithm

Sabarinath.G

Dept. of EEE, Sri Venkateswara University, Tirupathi, Pin: 517502, India E-mail: sabarinath204@gmail.com

Dr. T.Gowri Manohar

Dept. EEE, Sri Venkateswara University, Tirupathi, Pin: 517502, India E-mail: gsnphd@gmail.com

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Abstract—Indian practical rural distribution systems are very long and spread over a wide range of area. The nodes far away from the distribution substation are suffering from low voltage. In India, total distribution system losses are around 20% to 25%. From the past few years, penetration of distributed generation (DG) in to the distribution network/system is increasing expeditiously. DG allocation with appropriate location and size can provide numerous benefits to the distribution companies as well as to the society. In this regard, a new technique called combined sensitivity index (CSI), to find the optimal DG unit location, based on voltage sensitivity and network load magnitude is proposed. To assess the effectiveness of the proposed technique, it is tested on Indian practical 52-bus rural distribution system. The results obtained with the proposed CSI technique is compared with the results obtained with the combined power loss sensitivity (CPLS) technique. Here, the optimal DG unit size is calculated using Bird Swarm Algorithm (BSA). The results show that the proposed CSI technique performs better in minimizing power losses and voltage profile augmentation when compared to existing CPLS technique.

Index Terms—Bird swarm algorithm, Combined power loss sensitivity, Combined sensitivity index, Distributed generation, Distribution system, power loss, voltage deviation.

ABBREVIATIONS AND ACRONYMS

P _{totalloss}	Total real power loss	KVA _{DG}	Apparent power of DG
P _m	Real power flow from m th bus	KVA _{Load}	Apparent power of load
PL_k	Active power at node K	QL_k	Reactive load at node K
P_{m+1}	Real power flow from (m+1) th bus	V_{m}	Voltage of mth bus
P _{DG}	Real power of DG	$V_{m\!+\!1}$	Voltage of (m+1) th bus
P _{L.m+1}	Real load of (m+1)th	V _{rated}	Rated voltage

	bus		
Qm	Reactive load of m th bus	\mathbf{V}_{j}	Voltage at bus j
Q_{m+1}	Reactive load of (m+1) th bus	V_{j}^{min}	Minimum voltage at bus j
Q _{DG}	Reactive power of DG	$V_{j}^{max} \\$	Maximum voltage at bus j
$Q_{L,m+1} \\$	Reactive load of (m+1) th bus	$X_{m,m+1} \\$	Reactance of branch between m and (m+1) bus
$R_{m,m+1}$	Resistance of branch between m and (m+1) bus	X(j)	Reactance of branch j
R(j)	Resistance of branch j	nb	Number of buses

I. INTRODUCTION

Electrical energy distribution systems/networks are generally operated in radial configuration. Due to high resistance (R) / reactance (X) ratio [1], distribution networks cause a poor voltage regulation and considerable amount of power losses. And also as compared to transmission system, the distribution system (DS) is more complex in structure and is having more power loss due to low voltage and high current operating conditions. Major part of the load on DS is inductive in nature [2] and causes more power loss and poor voltage regulation. In the previous literature it is recorded that around 13% [3] of the total power production is lost in the DS as line losses. According to Indian records, distribution losses are around 21% [4]. From the past several years, power systems are transforming from centralized power generating state with power plants connected to the transmission system to the decentralized power generating state [5], with small power generating units directly connected to distribution systems. Minimization of such a high power loss and voltage regulation plays a vital role in distribution system planning, design and expansion [6]. Hence, it is essential to look towards the techniques that minimize the above drawbacks. Distributed / dispersed / decentralized generation [7] placement [1, 2, 4], network feeder re-configuration [3, 8-11], capacitor placement [12, 13] and load balancing [14] are the major techniques used for the power loss minimization and enhancement of system voltage. From the past couple of years, renewable energy based DG placement is being extensively used as it provides many technical, financial and ecological benefits [2]. DG technologies are broadly classified [15] into:

- Renewable energy based DGs comprise of small hydro, solar photovoltaic, wind, biomass, geothermal and so on.
- Fossil fuel/non-renewable energy based DGs comprise internal combustion engine, diesel engine, fuel cells and so on.

Another way of classifying DG technologies [16]:

Type-1 DG: It can produce active power but not reactive power. (Solar PV)

Type-2 DG: It can produce active as well as reactive power. (Synchronous generator)

Type-3 DG: It can produce active power and extracts reactive power. (Induction generator)

Type-4 DG: It can produce only reactive power. (Capacitor)

The remaining sections of this paper are arranged as follows: Section II explains related work. Section III presents problem formulation and system constraints. Section IV and V discuss about optimal power factor and proposed optimal DG location methods. Finally, sections VI and VII explain BSA and experimental results, respectively.

II. RELATED WORK

The placement of DG has a significant effect on distribution network performance. Unsuitable position of DG may cause increased capital investment, decreased performance of system. On the other hand the appropriate placement helps in minimization of network loss and improvement of system voltage profile. There are numerous analytical and optimization approaches utilized in the literature. Majority of analytical and optimization approaches are employed to find the optimal location and size of DG respectively. In [17-19] analytical approaches based on power loss sensitivity and power stability index have been proposed to find the optimal location and sizing of DGs in radial distribution systems. Various scientists and researchers have been introduced several meta-heuristic based optimization algorithms for solving optimal DG allocation problem. In [20] authors were employed three meta-heuristic algorithms including imperialist competitive algorithm (ICA) [20], genetic algorithm (GA) [20] and particle swarm optimization algorithm (PSO) [20], to solve optimal DG allocation problem. In [20] authors reported that PSO performed better than ICA and GA. PSO is used [21] to solve multiobjective problem including maximization of network loss, minimization of initial investment on DG, voltage

stability improvement and greenhouse emissions minimization considering time varying load. Multi objective chaotic symbiotic organisms search algorithm [22], whale optimization algorithm [23], flower pollination algorithm [24], improved multi-objective harmony search algorithm [25], grey wolf optimization algorithm [26] were employed.

III. PROBLEM FORMULATION & CONSTRAINTS

A. Problem Formulation

The main motive of this problem is to diminish the network power loss. The sum of total network loss is considered as fitness function and is calculated as

$$P_{total \, loss} = \min \sum_{m=1}^{nb} P_{loss}(m, m+1) \tag{1}$$

Where, nb=total number of nodes and $P_{loss}(m, m+1)$ =Real loss between mth node and (m+1)th node

B. Power Flow Constraints

The Real power eq. (2) and reactive power eq. (3) flow in each branch and end bus voltage eq. (4) are determined as follows [27]:

$$P_{m+1} = P_m + P_{DG} - P_{L,m+1} - R_{m,m+1} \times \frac{(P_m^2 + Q_m^2)}{|V_m|^2} \quad (2)$$

$$Q_{m+1} = Q_m + Q_{DG} - Q_{L,m+1} - X_{m,m+1} \times \frac{(P_m^2 + Q_m^2)}{|V_m|^2}$$
(3)

$$|V_{m+1}|^{2} = |V_{m}|^{2} - 2(R_{m,m+1} \times P_{m} + X_{m,m+1} \times Q_{m}) + (R_{m,m+1}^{2} + X_{m,m+1}^{2}) \times \frac{(P_{m}^{2} + Q_{m}^{2})}{|V_{m}|^{2}}$$
(4)

C. Voltage Limits

The magnitude of voltages of all buses should lie within the pre-specified range and is represented as

$$V_j^{\min} \le V_j \le V_j^{\max} \tag{5}$$

Where $V_i^{\min} = 0.9 \text{ p.u}$ and $V_i^{\max} = 1.05 \text{ p.u}$

IV. OPTIMAL POWER FACTOR

A fast approach [28] is considered to select the optimal power factor (P.F). Consider a simple two bus radial DS in Fig.1. The conceivable least power loss can be accomplished when the P.F of DG (PF_{DG}) is selected to be equal to that of total system connected load power

factor (PF_{load}). That can be represented by

$$PF_{DG} = PF_{load} \tag{6}$$



Fig.1. Simple two bus RDS with DG

The connected load P.F of the system $(\mbox{PF}_{\mbox{load}})$ is given by

$$PF_{load} = \frac{P_L}{\sqrt{P_L^2 + Q_L^2}}$$
(7)

The DG P.F is given by

$$PF_{DG} = \frac{P_{DG}}{\sqrt{P_{DG}^2 + Q_{DG}^2}}$$
(8)

Where

 P_L and P_{DG} are active power of load and DG. Q_L and Q_{DG} are reactive power of load and DG.

V. OPTIMAL DG PLACEMENT METHODS

These approaches are employed to find out the optimal nodes to place DG units and helps in minimization of search space while executing the optimization program.

A. Combined Power Loss Sensitivity (CPLS)

Total network losses depend not only on reactive power injection but also on real power injection. Hence, CPLS [19] is being planned by in view of both real, reactive power injections and the procedure is follows as below:

CPLS corresponding to active/real power injection is given by

$$\frac{\partial KVA_{loss}}{\partial KW_i} = \frac{\partial KW_{loss}}{\partial KW_i} + j\frac{\partial KVAr_{loss}}{\partial KW_i}$$
(9)

$$\frac{\partial KVA_{loss}}{\partial KW_i} = \frac{2 * KW_i * R(j)}{V_i^2} + j \frac{2 * KW_i * X(j)}{V_i^2} \quad (10)$$

CPLS corresponding to reactive power injection is

$$\frac{\partial KVA_{loss}}{\partial KVAr_i} = \frac{\partial KW_{loss}}{\partial KVAr_i} + j\frac{\partial KVAr_{loss}}{\partial KVAr_i}$$
(11)

$$\frac{\partial KVA_{loss}}{\partial KVAr_i} = \frac{2*KVAr_i*R(j)}{V_i^2} + j\frac{2*KVAr_i*X(j)}{V_i^2} \quad (12)$$

Combined Power Loss Sensitivity

$$= \frac{\left|\frac{\partial KW_{loss}}{\partial KW_{i}} \frac{\partial KVAr_{loss}}{\partial KW_{i}}\right|}{\left|\frac{\partial KW_{loss}}{\partial KVAr_{i}} \frac{\partial KVAr_{loss}}{\partial KVAr_{i}}\right|}$$
(13)

Where, R(j) and X(j) are resistance and reactance of line 'j', respectively. KW_{loss} and $KVAr_{loss}$ are active and reactive power loss, respectively. KW_i and $KVAr_i$ are active and reactive power injection, respectively, and V_i is voltage magnitude at bus 'i'.

Top most sensitive buses and normalized voltage magnitudes under 1.01 are selected to place DG. The normalized bus voltages are calculated as below

Normalized,
$$V(n) = V(n) / 0.95$$
 (14)

B. Combined Sensitivity Index

Proposed CSI [29] is employed to locate the most suitable nodes/buses to incorporate the DG units on an Indian practical 52-bus RDN. It mainly depends on

- Voltage sensitivity
- Apparent power of a connected load

CSI (S_b) is mathematically modeled as follows

$$S_b = \sum_{k=2}^{nb} V_{k,b} * KVA_k + \Delta V_b^{\max}$$
(15)

for b=2,3,4,.....nb

Note: Node '1' is not considered because it is substation node or reference node and nb= maximum number of nodes or buses.

The maximum change in voltage magnitude (ΔV_b^{max}) after the placement of DG unit is given as follows:

$$\Delta V_b^{\max} = \max |V_{k,b}^{act} - V_{k,b}^{base}|$$
(16)

Here, variables V_{kb}^{act} and V_{kb}^{base} are voltages at node 'b' after and before placement of DG at node 'k', respectively.

The KVA magnitude of connected load at bus 'k' is calculated as follows:

$$KVA_{k} = \sqrt{(PL_{k})^{2} + (QL_{k})^{2}}$$
 (17)

Here, PL_k and QL_k are active power magnitude and reactive power magnitude of connected load at node 'k'.

Ranking of buses in each feeder is obtained using eq. (15). The value of S_b is calculated at each bus (except reference bus) by injecting active power of 10%, 20% and 30% of total active power. Bus with highest S_b value should be selected as candidate bus to place DG unit.

VI. BIRD SWARM ALGORITHM

In this work, bird swarm algorithm (BSA) [30] is employed to determine the optimal DG capacity/size. BSA is a new optimization technique developed by authors in 2015. BSA is developed from the intelligence observed from the birds in swarm during communication and social behavior. In general, most of the birds exhibit three kinds of behaviors like foraging, vigilance and flight behaviors.

A. Foraging Behavior

All birds in the swarm quests for food based on its previous knowledge and swarms experience. These actions can be mathematically expressed as below:

$$X_{m,n}^{t+1} = X_{m,n}^{t} + (\mathbf{P}_{m,n} - x_{m,n}^{t}) \times C \times \operatorname{rand}(0,1) + (\mathbf{g}_{n} - X_{m,n}^{t}) \times S \times \operatorname{rand}(0,1)$$
(18)

In the above eq. (18), rand(0,1) denotes a randomly generated number between (0,1) and n [1,2,...,D]. S and C are respectively named as social accelerated and cognitive accelerated coefficients and both are positive numbers. $P_{m,n}$ is the previous best position of m^{th} bird and g_n is the previous best position of a swarm.

B. Vigilance Behavior

Every bird in the swarm tries and competes with other birds in the swarm to get a position in the middle of the swarm to safeguard themselves from the predators. Hence, each bird in the swarm would not move continuously towards the center. The mathematical representation of these motions is as follows:

$$X_{m,n}^{t+1} = X_{m,n}^{t} + A1(mean_n - X_{m,n}^{t}) \times rand(0,1) + A2(P_{a,n} - X_{m,n}^{t}) \times rand(-1,1)$$
(19)

$$A1 = a1 \times \exp\left(-\frac{PFit_m}{sumFit + \varepsilon} \times \mathbf{N}\right)$$
(20)

$$A2 = a2 \times \exp\left(\left(\frac{PFit_m - PFit_q}{|PFit_q - PFit_m| + \varepsilon}\right) \frac{N \times PFit_q}{sumFit + \varepsilon}\right) (21)$$

Where q ($q \neq m$) is a randomly generated positive number between 1 and *N*. *a1* and *a2* are positive numbers in [0 2]. *PFit_m* represents the *mth* bird's best fitness value. *sumFit* denotes sum of the best fitness of all the birds in the swarm. ε is a small number to eliminate zerodivision error and *mean_n* represents n^{th} bird average position.

C. Flight Behavior

While searching food the birds move from one location to a different location due to predation threat or any other reason and once again at the arrived site they would forage for food. Some of the birds in the swarm called producers would quest for food patches while the rest of the swarm called scroungers try to forage the food patches identified by the producers. The mathematical representation of producer and scrounger behavior may be as follows:

$$X_{m,n}^{t+1} = X_{m,n}^{t} + randn(0,1) \times X_{m,n}^{t}$$
(22)

$$X_{m,n}^{t+1} = X_{m,n}^{t} + (X_{q,n}^{t} - X_{m,n}^{t}) \times FL \times rand(0,1)$$
(23)

Here, randn(0,1) represents Gaussian distributed random value with 0 and 1, respectively as mean and standard deviation and *FL* represents the following factor. The flow chart of the proposed BSA is shown in Fig. 2.



Fig.2. Flowchart of BSA

D. Implementation of BSA

The complete algorithm of the proposed method is as follows:

STEP: 1 Load line and load data of an Indian 52-bus distribution system to run power flow program.

STEP: 2 Identify the most suitable node/bus in each feeder using the CPLS and CSI approaches.

STEP: 3 Initialize population and other BSA parameters.

STEP: 4 Generate birds (DG sizes) using eq. (24)

$$DG Size = (DG_{max} - DG_{min}) * rand() + DG_{min}$$
(24)

STEP: 5 Calculate the power loss of 52-bus distribution system for generated DG sizes

STEP: 6 Identify DG size with minimum power loss

STEP: 7 Update DG sizes using eq. (18) - eq. (23)

STEP: 8 Calculate power losses for updated DG sizes

STEP: 9 Update current best DG size if the power loss obtained in step 8 is less than power loss obtained in step 5 otherwise moves to step 7.

STEP: 10 Stop if the criterion is satisfied

VII. EXPERIMENTAL RESULTS

The Indian practical radial distribution system portrayed in [31] is considered for evaluation of proposed technique. The line and load information [32] about this considered test system is presented in appendix. This test system consists of 3 main feeders, 52 buses and 51 branches feeding a total network load of (4184+j2025) KVA. The power factor of connected load of this test system is 0.9 lagging. The base KV and KVA for this considered test system are considered as 11 and 1000, respectively. The maximum and minimum bus voltage magnitude limits for the given test system are 1.05p.u and 0.9 p.u., respectively. For Indian 52-bus practical distribution system without integration of DG unit, total active and reactive losses are (887.19+j381.69) KVA. Total active and reactive power injection from the substation is (5071.19+j2406.69) KVA. The vital objective of this work is minimization of network loss and total load voltage deviation. The maximum number of DG units installed for this system is considered to be equal to number of feeders i.e. 3. The simulation programed of this proposed BSA is developed in MATLAB R2014a environment. During simulation, the following BSA parameters are considered: number of birds/population, N=30; maximum iterations=50; bird's flight behavior frequency, FQ=10; constants, a1=a2=1; C=S=1.5.

Table 1. Specifications of Indian practical 52-bus RDN

Base KVA	Pasa KV	Connec	cted load	Power loss KW KVAr	
	Dase K v	KW	KVAr	KW	KVAr
1000	11	4184	2025	887.19	381.69

While simulating the given test system, two dissimilar scenarios and three cases in each scenario are considered.

- Scenario-1: DG locations are determined with CPLS analysis.
- Scenario-2: DG locations are determined with CSI analysis.

In each scenario the following three case studies are analyzed.

- ✓ Case-1: Three DG units injecting active power only i.e. operating at Unity power factor, for instance, fuel cells, solar photovoltaic.
- ✓ Case-2: Three DG units injecting both active and reactive power and operating at 0.95 power factor, for instance, synchronous generator.
- ✓ Case-3: Three DG units injecting both active and reactive power and operating at 0.9 power factor (Optimal power factor).
- A. Scenario-1

In scenario-1, bus locations in each feeder to incorporate DG units are determined using CPLS analysis. CPLS values and normalized voltages of all buses are determined using eq. (13), (14) and are graphically presented in Fig. 3 and Fig. 4, respectively. Now, the buses/nodes are arranged in descending order based on CPLS value. Top 5 sensitive nodes with its normalized voltages less than 1.01 are recorded in Table 2. The top ranked nodes i.e. 18, 23 and 44 are picked first for DG unit placement.







Fig.4. Normalized voltage profile of test system

Pople of hus		Bus number				
Kalik of bus	Feeder-1	Feeder-2	Feeder-3			
1	18	23	44			
2	3	24	33			
3	13	26	36			
4	17		50			
5	15		46			

Case-1: In case-1, three type-1 DG units operating at unity P.F are installed at nodes 18, 23 and 44. The results achieved in this case are provided in Table 3. After placing three DG units of capacities 752.42KVA (18), 457.53KVA (23) and 1054.12KVA (44), active power losses (Σ KW loss) are reduced from 887.19 KW to 310.62KW and reactive power losses (Σ KVAr loss) from 381.69KVAr to 133.81KVAr. Similarly, the active and reactive power supplied by substation is reduced from (5071.19+j2406.69) KVA to (2230.92+j2158.81) KVA.

Table 3. Optimization results of scenario-1

particulars	Base case	Case-1	Case-2	Case-3
ΣKW loss	887.194	310.62	219.67	211.31
ΣKVAr loss	381.69	133.81	94.51	90.91
DG location		752.42	878.54	875.74
and size		457.53	452.29	466.62
(KVA)		1054.1	1147.8	1162.25
Vmin (p.u)	0.6844	0.87093	0.90033	0.90313
Σ Vdevi	8.5796	3.2649	2.2850	2.2278

Fig. 5 shows the voltage profile of test system. From Fig. 5 it is very clear that there is a considerable improvement in voltage profile from base case to case-1. In this case the minimum voltage level (|Vmin|) is improved from 0.6844p.u to 0.87093p.u and total load

voltage deviation (Σ |Vdevi|) is reduced from 8.5796 to 3.2649.

Case-2: In case-2, three type-2 DG units injecting both active and reactive power at 0.95 P.F are placed at nodes 18, 23 and 24. The optimal results obtained with this case are recorded in Table 3. By installing three DG units with its optimal capacities of 878.54KVA (18), 452.29KVA (23) and 1147.85KVA (44), the active losses are minimized to 219.67KW and reactive losses to 94.51KVAr. In this case the power injected from substation is minimized from (5071.19+j2406.69) KVA to (2075.66+j1354.39) KVA. The voltage profile of this case is portrayed in Fig. 5. From Fig. 5 it is clear that the voltage profile is significantly improved when compared to above two cases i.e. base case and case-1. In this case, |Vmin| is improved from 0.6844p.u to 0.9003p.u and Σ |Vdevi| is reduced from 8.5796 to 2.285. From Fig. 2, it is also noticed that all nodes of test system are within the acceptable voltage limit i.e. in between 0.9p.u and 1.05p.u.

Case-3: Three type-2 DG units injecting both active and reactive power at 0.9 P.F (optimal P.F) are installed at nodes 18, 23 and 24 of Indian practical 52-bus urban distribution system. The obtained optimal numerical results are inserted in Table 3. The optimal size of DG units at nodes 18, 23 and 24 are found to be 875.74KVA 466.62KVA (23) and 1162.25KVA (44), (18)respectively. Case-3 of scenario-1 yields reduced active and reactive power loss of 211.KW and 90.91KVAr, respectively. The value of |Vmin| is improved from 0.6844p.u to 0.90313p.u. Total load voltage deviation is reduced to 8.5796 to 2.2278. From Fig. 5 it is clear that as compared to all cases, case-3 exhibits better voltage profile. This is because of increased reactive power injection from the DG units.



Fig.5. Voltage profile of test system with scenario-1

B. Scenario-2

In scenario-2, the locations of DG units are first finalized using the proposed CSI. The CSI values for DG

power injection of 10%, 20% and 30% of total active power load are graphically presented in Fig. 6. The top 5 ranked buses in each feeder concerning CSI are recorded in Table 4. From Table 4 nodes 19, 24 and 50 are selected to incorporate DG units in this scenario.

Table 4. Ranking of nodes using combined sensitivity index

	I	Feeder-	1	Feeder-2			I	Feeder-3	
Rank	DG power			DG power			DG power		
of bus	inje	ction (%	% of	injection (% of TRPL)		injection (% of TRPL)			
cus	10	20	30	10	20	30	10	20	30
1	19	19	19	24	24	24	50	50	50
2	18	18	18	26	26	26	52	52	52
3	17	17	17	23	23	23	51	51	51
4	15	15	15	31	31	31	49	49	49
5	14	14	14	25	25	25	48	44	48

Case-1: In case-1 of scenario-2, three type-1 DG units injecting active power at unity P.F are installed at nodes 19, 24 and 50. The optimized numerical results attained in this case are provided in Table 5. After placing three DG units of capacities 694.01KVA (19), 367.41KVA (24) and 1060.59KVA (50), active power losses (ΣKW loss) are reduced from 887.19 KW to 293.78KW and reactive power losses (SKVAr loss) from 381.69KVAr to 126.39KVAr. Similarly, the active and reactive power substation is reduced supplied by from (5071.19+j2406.69) KVA to (2355.78+j2151.39) KVA. Fig. 7 shows the voltage profile of test system with scenario-2. From Fig. 7, it is very clear that there is a considerable improvement in voltage profile from base case to case-1. In this case the minimum voltage level (|Vmin|) is improved from 0.6844p.u to 0.89254p.u and

total load voltage deviation (Σ |Vdevi|) is reduced from 8.5796 to 3.096.



Fig.6. Combined sensitivity index of test system



Fig.7. Voltage profile of test system with scenario-2

Case-2: In case-2 of scenario-2, three type-2 DG units injecting both active and reactive powers at 0.95 P.F are installed at nodes 19, 24 and 50. The optimal numerical results obtained with this case are recorded in Table 5. By installing three DG units with its optimal capacities of 771.36KVA (19), 388.73KVA (24) and 1151.2KVA (50), the active losses are minimized to 202.55KW and reactive losses to 87.14KVAr. In this case, the power injected from substation is minimized from (5071.19+j2406.69) KVA to (2190.83+j1390.56) KVA.

The voltage profile of this case is portrayed in Fig.7. From Fig.7 it is clear that the voltage profile is significantly improved when compared to above two cases i.e. base case and case-1. In this case, |Vmin| is improved from 0.6844p.u to 0.91225p.u and $\Sigma|Vdevi|$ is reduced from 8.5796 to 2.1536. From Fig.7, it is also noticed that all nodes of test system are within the acceptable voltage limit i.e. in between 0.9p.u and 1.05p.u.

Particulars	Base case	Case-1	Case-2	Case-3
ΣKW loss	887.194	293.78	202.55	194.04
Σ KVAr loss	381.69	126.39	87.14	83.48
DG location		694.01	771.36	781.07
and size		367.41	388.73	402.91
(KVA)		1060.59	1151.20	1180.79
Vmin (p.u)	0.6844	0.89254	0.91225	0.91550
Σ Vdevi 8.5796		3.0960	2.1536	2.0391

Table 5. Optimization results of scenario-2

Case-3: Three type-2 DG units injecting both active and reactive powers at 0.9 P.F (optimal P.F) are installed at nodes 19, 24 and 55 of Indian practical 52-bus rural distribution system. The obtained optimal numerical results are inserted in Table 5. The optimal size of DG units at nodes 19, 24 and 50 are found to be 781.07KVA (19), 402.91KVA (24) and 1180.79KVA (50), respectively. Case-3 of scenario-2 yields reduced active and reactive power loss of 194.04KW and 83.48KVAr, respectively. The value of |Vmin| is improved from 0.6844p.u to 0.9155p.u. Total load voltage deviation is reduced to 8.5796 to 2.0391. From Fig. 7 it is clear that as compared to all cases of scenario-2, case-3 exhibits better voltage profile. This is because of increased reactive power injection from the DG units.

Fig. 8 shows the convergence curves of a proposed BSA for solving the optimal DG allocation problem. From Fig. 8, it is clear that BSA has good convergence speed.



Fig.8. Convergence curves of proposed BSA

VIII. CONCLUSIONS

In this work, an optimal DG allocation problem on Indian practical 52-bus radial distribution system was solved. Here, CPLS and CSI were used to determine the DG locations. A new algorithm called bird swarm algorithm (BSA) was used to calculate the optimal DG size. The results obtained with CPLS and CSI methods are compared. From the results it is observed/concluded that, the least values of power loss and total voltage deviation are achieved with minimum DG size in scenario-2. The results achieved with scenario-2 are as follows: Total active power loss reduction of 66.88%, 77.16% and 78.12% were achieved in Case 1, 2 and 3, respectively. Total voltage deviation reduction of 63.91%, 74.89% and 76.23% were achieve with case 1, 2 and 3, respectively.

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APPENDIX

Specifications of an Indian practical 52-bus RDS

S. No.	From bus	To bus	R (p.u)	X (p.u)	P(KW)	Q (KVAr)
1	1	2	0.0258	0.01110	81	39
2	2	3	0.0430	0.01850	135	65
3	2	4	0.0129	0.00555	108	52
4	4	5	0.0129	0.00555	108	52
5	4	6	0.0086	0.00370	27	13
6	6	7	0.0172	0.00740	54	26
7	6	8	0.0215	0.00925	135	65
8	8	9	0.0258	0.01110	81	39
9	9	10	0.0430	0.01850	67	32
10	10	11	0.0129	0.00555	27	13
11	11	12	0.0086	0.00370	27	13
12	11	13	0.0430	0.01850	108	52
13	12	14	0.0301	0.01295	54	26
14	12	15	0.0344	0.01480	94	45
15	10	16	0.0129	0.00555	67	33
16	16	17	0.0516	0.02220	67	33
17	16	18	0.0430	0.01850	108	52
18	18	19	0.0344	0.01480	81	39
19	1	20	0.0086	0.00370	108	52
20	20	21	0.0129	0.00555	94	46
21	21	22	0.0258	0.01110	81	39
22	22	23	0.0430	0.01850	108	52
23	23	24	0.0215	0.00925	108	52
24	22	25	0.0258	0.01110	102	50
25	25	26	0.0344	0.01480	41	20
26	20	27	0.0086	0.00370	108	52
27	27	28	0.0129	0.00555	162	79
28	28	29	0.0215	0.00925	68	33
29	27	30	0.0344	0.01480	68	33
30	30	31	0.0430	0.01850	95	46
31	1	32	0.0344	0.01480	41	20
32	32	33	0.0430	0.01850	121	59
33	33	34	0.0344	0.01480	41	20
34	33	35	0.0301	0.01295	41	20
35	35	36	0.0344	0.01480	135	66
36	36	37	0.0215	0.00925	81	40
37	35	38	0.0172	0.00740	68	33
38	33	39	0.0215	0.00925	95	46
39	39	40	0.0172	0.00740	108	52
40	39	41	0.0215	0.00925	41	20
41	41	42	0.0258	0.01110	95	46
42	41	43	0.0387	0.01665	27	13
43	43	44	0.0430	0.01850	122	59
44	41	45	0.0129	0.00555	108	52
45	45	46	0.0301	0.01295	81	39
46	45	47	0.0215	0.00925	68	33
47	47	48	0.0129	0.00555	41	20
48	47	49	0.0129	0.00555	68	33
49	49	50	0.0344	0.01480	81	39
50	49	51	0.0129	0.00555	108	52
51	51	52	0.0086	0.00370	41	20

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Authors' Profiles



Sabarinath.G received his B.Tech and M.Tech degrees in Electrical and Electronics Engineering from JNT University Anantapuramu, India, in 2009 and 2013, respectively. Currently, he is pursuing his Ph.D. in the Department of Electrical and Electronics Engineering at the S.V.

University, Tirupati. His research interests are in the areas of Soft computing techniques, Artificial neural networks, FACTS, Nature-inspired algorithms, Economic load dispatch, Renewable energy sources, and Power electronics.



Dr. T. Gowri Manohar received his B.Tech, M.Tech and Ph.D. degrees from S.V. University, Tirupati, India, in 1996, 1998 and 2007 respectively. Currently, he is working as a professor in the department of EEE, SV University, Tirupati. His current research areas include power quality issues, FACTS

technology, distributed energy resources and the application of artificial intelligent techniques on power systems.

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