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Effects of Superstrate on Electromagnetically and Gap Coupled Patch Antennas

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Abstract

In this paper the effects of water loading (termed as superstrate) on the characteristics of an electromagnetically (EM) and coupled pentagonal patch antennas operating in the ISM band have been described. The proposed antenna structures are analyzed using HFSS and the influence of the superstrate on resonant frequency, bandwidth, VSWR and radiation characteristics have also been analyzed. The obtained results also reveal that a larger bandwidth can be found in case the dielectric substrate is separated by air gap spacing. In addition, though impedance matching is little deteriorated due to loading, however the operating frequency band (BW) shifted to lower side significantly.

Index Terms: Electromagnetically coupled (EMC), electromagnetically gap coupled (EMGC), microstrip patch antenna, stacked antenna, pentagonal patch antenna.

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1. Introduction

Generally during rainy environments water may easily get accumulated over the surface of patch antennas being used in the open atmosphere. Hence exposure of patch antenna to the snow fall and buildup of snow or ice over its patch surface, or exposure to rain water and accumulation of water over its patch surface should be taken into account during the design phase. For a microstrip patch antenna which is a narrow band device exposure to such environmental conditions causing its resonant frequency getting lowered [1, 2]. Effect of dielectric superstrate on parameters such as resonant frequency, input impedance, radiation efficiency, etc. for single element microstrip patch antenna is already reported in the literature [3–6]. In past many researchers have worked on electromagnetically coupled patch antenna; First Q. Rao presented an electromagnetically

* Corresponding author. Email address: ravipusad@gmail.com coupling fed broadband low profile microstrip antenna (MSA) array [7]. Radiating element is an E-shaped MSA that is fed by an electromagnetically coupled strip and covered by a low loss radome. In September 2007, Deosarkar *et al.* designed high gain two-layer electro-magnetically coupled patch antenna in the ISM band [8]. Latter, in March 2008, Ikeda enhanced bandwidth of a low profile microstrip antenna which is electromagnetically coupled with a Folded Inverted *L*-shaped Probe [9]. However, Lee *et al.* have described and characterized, an electromagnetic coupled patch antenna covered with superstrate and found that for the antenna operating in the high-gain region, the resonant input impedance increases and the 3 dB beam-width decreases with the dielectric thickness [10-12]. F.R. Cooray and J.S. Kot has analyzed radiation of a cylindrical-rectangular microstrip patch antenna loaded with a superstrate and an air gap between the substrate and the superstrate, using the full-wave approach as well as the electric surface current model. They presented the results in the form of normalized radiation patterns for various thicknesses of the air gap and for superstrate made of lossy dielectric material [13].

However, the effects of a water as superstrate on the centre frequency and bandwidth of electromagnetic coupled and gap coupled pentagonal patch antenna have not yet studied though both structures shows significant alteration in their performances. Therefore, authors have made an attempt to investigate and describe the effects of the water layers on the surface of the electromagnetically and gap coupled probe fed pentagonal antennas.

2. Design of Proposed Patch Antennas

2.1. Design of pentagonal antenna

In general the major advantages of a pentagonal patch antenna over the rectangular patch antenna that, it supports both linear and circular polarizations [14]. The pentagonal patch antenna provides circular polarization with only one feed where as rectangular patch antenna requires multiple feeds to get circular polarization. Hence a probe fed pentagonal antennas is chosen here for study because of its better impedance matching. The pentagonal antenna size calculations were done considering the invariance of the electrostatic energy below the pentagonal and circular patches, however maintaining their areas remain constant. Fig. 1 shows the geometry of a regular pentagonal shape, however the design specifications are given in Table 1.



Fig. 1 Geometry of a regular pentagonal shape

The relationship between the circles (r_1) to the side arm of the regular pentagon (r_2) is given in equation (1).

$$r_2^2 = \frac{\pi r_1^2}{2.37} \tag{1}$$

Side arm of the pentagon $(r_2) = 1.175 r_1$

In the derivation of the equation (1), the pentagonal patch is assumed to be a resonant cavity with perfectly conducting side walls. Because a circular disc is the limiting case of the polygon with large number of sides, in this case number of sides are 5. The resonant frequency of the dominant as well as for the higher order modes can be calculated from the formula given below [15]:

$$f_{np} = \frac{X'_{np}c}{2\pi r_{l}\sqrt{\mathcal{E}_{r}}}$$
(2)

Where X'_{np} are the zeros of the derivative of the Bessel function $J_n(x)$ of the order *n*, as is true for *TE* mode circular waveguides, however for the lowest order modes;

$$X'_{np} = 1.84118$$
 (3)

The lengths of each side of the pentagonal antenna are calculated by using equations (1) & (2). For coaxial feed, the location of the feed point is usually selected to provide a good impedance match. The schematic of a pentagonal patch antenna is shown in Fig. 1 and design specifications are given in Table 1.

Table 1. Design parameters of the proposed antennas

Parameters	Electromagnetically coupled antenna	EMC gap coupled antenna (gap size,d =0.4 mm)
Designed frequency (GHz)	2.39	2.41
Substrate 1(FR-4)	$\varepsilon_{rl} = 4.4, tan\delta = 0.02,$	$\varepsilon_{rl} = 4.4, tan\delta = 0.02,$
	$h_1=0.8 \text{ mm}$	$h_1 = 0.8 \text{ mm}$
Size of the pentagon $(l_1 = l_2)$	28.52 mm	28.52 mm
Substrate 2(Plexiglas)	$\varepsilon_{r2} = 3.4, tan\delta = 0.001, h_2 = 0.8 \text{ mm}$	$\varepsilon_{r2} = 3.4, tan\delta = 0.001, h_2 = 0.8$
		mm
Dielectric cover(Water)	$\varepsilon_r = 81, tan\delta = 0.0$	$\varepsilon_r = 81$, $tan\delta = 0.0$
Feed location	9.0 mm from the centre	9.0 mm from the centre

2.2. Design of electromagnetically coupled patch antenna geometry

The side views of the proposed antennas are shown in the Fig. 2 (a & b). The lower pentagonal patch is fed by a coaxial cable and upper pentagonal patches are coupled through the fringing field.



Fig. 2a Schematic diagram of electromagnetically coupled patch antenna



Fig. 2b Schematic diagram of electromagnetically coupled patch antenna with dielectric cover (water layer)

However the photograph of fabricated electromagnetic coupled patch antenna surface with feed line and pentagonal patch antenna are shown in Fig.3.



Fig. 3 Structure of electromagnetically coupled patch antenna fed with coaxial feed

2.3. Design of electromagnetically gap coupled antenna geometry

The geometry of the electromagnetic gap coupled patch antennas are shown in Fig. 4a &b. The dimension of the side arm of the pentagonal patch antenna is l_1 and l_2 . The thickness of the lower substrate is h_1 and the permittivity is ε_{r1} while h_2 and ε_{r2} are the substrate thickness and permittivity of the upper patch respectively. The two patches are also separated by an air gap having a distance of *d* that can be adjusted to 0.4 mm.



Fig. 4(a) Schematic diagram of electromagnetically gap coupled patch antenna

Fig. 4 (b) Schematic diagram of electromagnetically gap coupled patch antenna with water layer

However the photograph of fabricated electromagnetic gap coupled patch antenna surface with feed line are shown in Fig. 5.



Fig. 5 Fabricated prototype of electromagnetically gap coupled patch antenna

3. Results and Discussions

The results of observed return loss (dB) against frequency over the operating band of the EM coupled antenna are plotted in Fig. 6 in which t = 0 represents an antenna without any layer while t = 0.1, 0.2 and 0.3 mm represents the thickness of the water layer poured on the patch surface. It can be observed from this figure that there is change in return loss over the entire frequency band due to the change in the water layer superstrate thickness (0.1 mm to 0.3 mm). However, the centre frequency and the bandwidth are also slightly changed. So, we can conclude that EM coupled antennas loaded with dielectric superstrate like water, which has very high dielectric constant, show relative change in the resonant frequency. The obtained results are also summarised in Table 2. A network analyser is used for measurements of the S-parameter and the measured results are in excellent agreements with the simulated results, which is shown in the Fig. 6 and summarized in Table 3. From the Fig. 7, it is observed that, though impedance matching is little deteriorated, the operational frequency band will be slightly changed.



Fig. 6 Comparisons of return loss characteristics of the electromagnetically coupled patch antenna



Fig. 7 Comparisons of Input Impedance EM Coupled patch antenna

Table 2 Simulated parameters of the proposed electromagnetically coupled patch antenna

Types	Electromagnetically coupled antenna			
	Without dielectric cover	With dielectric cover		
		t = 0.1 mm	t = 0.2 mm	t = 0.3 mm
Designed frequency (GHz)	2.39	2.3	2.27	2.26
Return loss(dB)	-26.83	-16.84	-15.54	-14.2
Impedance (Ω)	47.15	40.06	37.12	33.9
VSWR	1.095	1.335	1.401	1.484
BW (MHz)	62.3	53.8	48.8	47.2
Gain	0.89208	1.1577		
Radiated Power(mW)	19.408	116.14		

Table 3 Measured parameters of the proposed electromagnetically coupled patch antenna

Types	Electromagnetically coupled antenna		
	Without dielectric cover	With dielectric cover with thickness $t = 0.1 \text{ mm}$	
Designed frequency (GHz)	2.39	2.3	
Return loss(dB)	-21.90	-30.80	
Band Width(MHz)	60	60	

The results of EM gap coupled antenna also reveals that return loss (dB) against frequency over the operating band of the antenna are plotted in Fig. 8 in which t = 0 represents an antenna without any layer while t = 0.1, 0.2 and 0.3 mm are the thickness of the water layer poured on the patch surface. It can be observed from this figure that there is change in return loss over the entire frequency band due to the change in the water layer superstrate thickness (0.1 mm to 0.3 mm). The variation of the resonant frequency of the antenna can be explained by the variation of the effective permittivity with accumulation of the water level on the surface of the antenna. The obtained results are also summarised in Table 4 which shows that the accumulation of the water level on the surface of the patch antenna parameters such as

return loss, impedance, VSWR, etc. A network analyser from Agilent TechnologiesTM is used for measurements and the measured results are slightly different from simulated results, which is shown in the Fig. 8 and summarized in Table 5. The difference in the measure and simulated result are minimized by accurate measurement of water layer thickness on the patch surface and by uniform distribution of water layer on the patch surface. From the Fig. 9, it is observed that, though impedance matching is little deteriorated, the operating frequency band will be slightly changed.



Fig. 8 Comparisons of return loss characteristics of the electromagnetically gap coupled patch antenna



Fig. 9 Comparison of Input Impedance of electromagnetically gap coupled patch antenna

Table 4 Simulated parameters of the proposed electromagnetically gap coupled patch antenna

Types	Electromagnetically coupled antenna			
	Without	With dielectric cover		
	dielectric cover	t = 0.1 mm	t = 0.2 mm	t = 0.3 mm
Designed frequency (GHz)	2.39	2.3	2.27	2.26
Return loss(dB)	-26.83	-16.84	-15.54	-14.2
Impedance (Ω)	47.15	40.06	37.12	33.9
VSWR	1.095	1.335	1.401	1.484
BW (MHz)	62.3	53.8	48.8	47.2
Gain	0.89208	1.1577		
Radiated Power(mW)	19.08	116.14		

Types	Electromagnetically Gap coupled antenna		
	Without dielectric cover	With dielectric cover with thickness t = 0.1 mm	
		2.22	
Designed frequency (GHz)	2.39	2.23	
Return loss(dB)	-25.3	-8.1	
BW(MHz)	70	0	

Table 5 Measured parameters of the proposed electromagnetically Gap coupled patch antenna

4. Conclusion

The behaviour of the EM couple and EM gap coupled patch antenna operating in ISM band due to the formation of a water layer superstrate on its surface is investigated. It is found that the bandwidth remains practically unaffected due to rain water accumulation on the patch surface. However, the exact value of return loss, at any particular frequency within the bandwidth, undergoes change which needs to be taken into account during system design. Analysis also shows that for t = 0.3 mm, antenna structure totally stops responding as bandwidth is almost goes zero. So, one may conclude that accumulation of rain water on the top of the antenna surface (EM coupled and EM gap coupled) makes them prone to frequency shift as well as impedance mismatch. So effects of environmental conditions should be taken into account during the design phase of an antenna. If due care is not taken during the design phase, the system may fail to respond as per requirement.

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